## Data Sheet

## FEATURES

High accuracy over line and load: $\pm 0.9 \%$ at $25^{\circ} \mathrm{C}, \pm 1.8 \%$ over temperature
Ultralow dropout voltage: $\mathbf{2 0 0} \mathbf{~ m V}$ (typical) at $\mathbf{5 0 0} \mathbf{~ m A}$
Requires only $\mathrm{C}_{0}=1.0 \boldsymbol{\mu}$ for stability
anyCAP ${ }^{\circledR}=$ stable with any type of capacitor (including MLCC)
Current and thermal limiting
Low noise
Low shutdown current: < 10 nA (typical)
2.6 V to 12 V supply range
$-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ambient temperature range

## APPLICATIONS

PCMCIA cards<br>Cellular phones<br>Camcorders, cameras<br>Networking systems, DSL/cable modems<br>Cable set-top box<br>MP3/CD players<br>DSP supplies

## GENERAL DESCRIPTION

The ADP3335 is a member of the ADP333x family of precision, low dropout, anyCAP voltage regulators. It operates with an input voltage range of 2.6 V to 12 V , and delivers a continuous load current up to 500 mA . The ADP3335 stands out from conventional low dropout regulators (LDOs) by using an enhanced process enabling it to offer performance advantages beyond its competition. Its patented design requires only a $1.0 \mu \mathrm{~F}$ output capacitor for stability. This device is insensitive to output capacitor equivalent series resistance (ESR), and is stable with any good quality capacitor-including ceramic (MLCC) types for space-restricted applications. The ADP3335 achieves exceptional accuracy of $\pm 0.9 \%$ at room temperature and $\pm 1.8 \%$ over temperature, line, and load.

## COMPARABLE PARTS

View a parametric search of comparable parts.

## DOCUMENTATION

## Application Notes

- AN-1072: How to Successfully Apply Low Dropout Regulators
- AN-262: Low-Noise Low Drop-Out Regulator for Portable Equipment


## Data Sheet

- ADP3335: High Accuracy Ultralow $\mathrm{I}_{\mathrm{Q}}, 500 \mathrm{~mA}$ anyCAP Low Dropout Regulator Data Sheet


## User Guides

- UG-461: ezLINX iCoupler Isolated Interface Development Environment Software User Guide


## TOOLS AND SIMULATIONS

- ADI Linear Regulator Design Tool and Parametric Search
- ADIsimPower ${ }^{T M}$ Voltage Regulator Design Tool


## DESIGN RESOURCES

- ADP3335 Material Declaration
- PCN-PDN Information
- Quality And Reliability
- Symbols and Footprints


## DISCUSSIONS

View all ADP3335 EngineerZone Discussions.

## SAMPLE AND BUY

Visit the product page to see pricing options.

## TECHNICAL SUPPORT $\square$

Submit a technical question or find your regional support number.

## DOCUMENT FEEDBACK

Submit feedback for this data sheet.

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## SPECIFICATIONS

All limits at temperature extremes are guaranteed via correlation using standard statistical quality control (SQC) methods. Ambient temperature of $85^{\circ} \mathrm{C}$ corresponds to a junction temperature of $125^{\circ} \mathrm{C}$ under pulsed full-load test conditions. Application stable with no load. $\mathrm{V}_{\text {IN }}=6.0 \mathrm{~V}, \mathrm{C}_{\text {IN }}=\mathrm{Cout}=1.0 \mu \mathrm{~F}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted.

Table 1.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OUTPUT |  |  |  |  |  |  |
| Voltage Accuracy ${ }^{1}$ | $V_{\text {OUT }}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {OUt(NOM) })}+0.4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ | -0.9 |  | +0.9 | \% |
|  |  | $\begin{aligned} & \mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {out(NOM })}+0.4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \\ & \mathrm{~T}_{\mathrm{A}}=85^{\circ} \mathrm{C} \end{aligned}$ | -1.8 |  | +1.8 | \% |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {OUt(NOM })}+0.4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \\ & \mathrm{~T}_{J}=150^{\circ} \mathrm{C} \end{aligned}$ | -2.3 |  | +2.3 | \% |
| Line Regulation ${ }^{1}$ |  | $\begin{aligned} & \mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {out(NOM) }}+0.4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 0.04 |  | $\mathrm{mV} / \mathrm{V}$ |
| Load Regulation |  | $\begin{aligned} & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 0.04 |  | $\mathrm{mV} / \mathrm{mA}$ |
| Dropout Voltage | V ${ }_{\text {drop }}$ | $\mathrm{V}_{\text {out }}=98 \%$ of $\mathrm{V}_{\text {out(Noм) }}$ |  |  |  |  |
|  |  | $\mathrm{L}_{\mathrm{L}}=500 \mathrm{~mA}$ |  | 200 | 370 | mV |
|  |  | $\mathrm{L}_{\mathrm{L}}=300 \mathrm{~mA}$ |  | 140 | 230 | mV |
|  |  | $\mathrm{LL}=50 \mathrm{~mA}$ |  | 30 | 110 | mV |
|  |  | $\mathrm{L}_{\mathrm{L}}=0.1 \mathrm{~mA}$ |  | 10 | 40 | mV |
| Peak Load Current | ILDPK | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OUT(NOM }}+1 \mathrm{~V}$ |  | 800 |  | mA $\mu \mathrm{V}$ rms |
| Output Noise | $\mathrm{V}_{\text {NOISE }}$ | $\mathrm{f}=10 \mathrm{~Hz}$ to $100 \mathrm{kHz}, \mathrm{C}_{\mathrm{L}}=10 \mu \mathrm{~F}$ |  | 47 |  |  |
|  |  | $\begin{aligned} & \mathrm{L}_{\mathrm{L}}=500 \mathrm{~mA}, \mathrm{C}_{\mathrm{NR}}=10 \mathrm{nF} \\ & \mathrm{f}=10 \mathrm{~Hz} \text { to } 100 \mathrm{kHz}, \mathrm{C}_{\mathrm{L}}=10 \mu \mathrm{~F} \\ & \mathrm{I}_{\mathrm{L}}=500 \mathrm{~mA}, \mathrm{C}_{\mathrm{NR}}=0 \mathrm{nF} \end{aligned}$ |  | 95 |  | $\mu \mathrm{V}$ rms |
| GROUND CURRENT |  |  |  |  |  |  |
| In Regulation | IGnd | $\mathrm{L}_{\mathrm{L}}=300 \mathrm{~mA}$ |  | 2.6 | 6 | mA |
|  |  | $\mathrm{L}_{\mathrm{L}}=50 \mathrm{~mA}$ |  | 0.5 | 2.5 | mA |
|  |  | $\mathrm{L}=0.1 \mathrm{~mA}$ |  | 80 | 110 | $\mu \mathrm{A}$ |
| In Dropout | Ignd | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {out(NoM) }}-100 \mathrm{mV} \\ & \mathrm{I}_{\mathrm{L}}=0.1 \mathrm{~mA} \end{aligned}$ |  | 120 | 400 | $\mu \mathrm{A}$ |
| In Shutdown | $1{ }_{\text {GNDSD }}$ | $\overline{\mathrm{SD}}=0 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=12 \mathrm{~V}$ |  | 0.01 | 1 | $\mu \mathrm{A}$ |
| SHUTDOWN |  |  |  |  |  |  |
| Threshold Voltage | $\mathrm{V}_{\text {THSD }}$ | ON | 2.0 |  |  | V |
|  |  | OFF |  |  | 0.4 | V |
| $\overline{\text { SD }}$ Input Current | ${ }_{\text {ISD }}$ | $0 \leq \overline{S D} \leq 5 \mathrm{~V}$ |  | 1.2 | 3 | $\mu \mathrm{A}$ |
| Output Current in Shutdown | IOSD | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=0 \mathrm{~V}$ |  | 0.01 | 5 | $\mu \mathrm{A}$ |

[^0]
## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :---: | :---: |
| Input Supply Voltage | -0.3 V to +16 V |
| Shutdown Input Voltage | -0.3 V to +16 V |
| Power Dissipation | Internally Limited |
| Operating Ambient Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Operating Junction Temperature Range | $-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| $\theta_{\text {JA, }}$ 2-layer MSOP-8 | $220^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\theta_{\text {JA, }}$, 4-layer MSOP-8 | $158^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\theta_{\text {JA, }}$, 2-layer LFCSP-8 | $62^{\circ} \mathrm{C} / \mathrm{W}$ |
| OJA, $^{\text {4-layer LFCSP-8 }}$ | $48^{\circ} \mathrm{C} / \mathrm{W}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering 10 sec ) | $300^{\circ} \mathrm{C}$ |
| Vapor Phase (60 sec) | $215^{\circ} \mathrm{C}$ |
| Infrared (15 sec) | $220^{\circ} \mathrm{C}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 3. 8-Lead MSOP


Figure 4. 8-Lead LFCSP

Table 3. Pin Function Descriptions

| Pin No. | Mnemonic | Function |
| :--- | :--- | :--- |
| $1,2,3$ | OUT | Output of the Regulator. Bypass to ground with a $1.0 \mu \mathrm{~F}$ or larger capacitor. All pins must be connected together <br> for proper operation. <br> Ground Pin. |
| 5 | GND | NR <br> 6 |
| Noise Reduction Pin. Used for further reduction of output noise (see the Noise Reduction section for further <br> details). |  |  |
| EP | IN | Active Low Shutdown Pin. Connect to ground to disable the regulator output. When shutdown is not used, this <br> pin should be connected to the input pin. <br> Regulator Input. All pins must be connected together for proper operation. |
| Pad |  |  |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 5. Line Regulation Output Voltage vs. Supply Voltage


Figure 6. Output Voltage vs. Load Current


Figure 7. Ground Current vs. Supply Voltage


Figure 8. Ground Current vs. Load Current


Figure 9. Output Voltage Variation vs. Junction Temperature


Figure 10. Ground Current vs. Junction Temperature


Figure 11. Dropout Voltage vs. Output Current


Figure 12. Power-Up/Power-Down


Figure 13. Power-Up Response


Figure 14. Line Transient Response


Figure 15. Line Transient Response


Figure 16. Load Transient Response


Figure 17. Load Transient Response


Figure 18. Short-Circuit Current


Figure 19. Turn On/Turn Off Response


Figure 20. Power Supply Ripple Rejection


Figure 21. RMS Noise versus $C_{L}(10 \mathrm{~Hz}$ to 100 kHz$)$


Figure 22. Output Noise Density

## THEORY OF OPERATION

The ADP3335 uses a single control loop for regulation and reference functions. The output voltage is sensed by a resistive voltage divider, R1 and R2, which is varied to provide the available output voltage option. Feedback is taken from this network by way of a series diode, D1, and a second resistor divider, R3 and R4, to the input of an amplifier.


Figure 23. Functional Block Diagram
A very high gain error amplifier is used to control this loop. The amplifier is constructed in such a way that equilibrium produces a large, temperature proportional input offset voltage that is repeatable and very well controlled. The temperature proportional offset voltage combines with the complementary diode voltage to form a virtual band gap voltage implicit in the network, although it never appears explicitly in the circuit.

This patented design makes it possible to control the loop with only one amplifier. This technique also improves the noise characteristics of the amplifier by providing more flexibility in the trade-off of noise sources that leads to a low noise design.
The R1 and R2 divider is chosen in the same ratio as the band gap voltage to the output voltage. Although the R1 and R2 resistor divider is loaded by the D1 diode and a second divider-R3 and

R4, the values can be chosen to produce a temperature stable output. This unique arrangement specifically corrects for the loading of the divider, thus avoiding the error resulting from base current loading in conventional circuits.
The patented amplifier controls a new and unique noninverting driver that drives the pass transistor, Q1. This special noninverting driver enables the frequency compensation to include the load capacitor in a pole-splitting arrangement to achieve reduced sensitivity to the value, type, and ESR of the load capacitance.

Most LDOs place very strict requirements on the range of ESR values for the output capacitor, because they are difficult to stabilize due to the uncertainty of load capacitance and resistance. The ESR value required to keep conventional LDOs stable, moreover, changes depending on load and temperature. These ESR limitations make designing with LDOs more difficult because of their unclear specifications and extreme variations over temperature.

With the ADP3335, ESR limitations are no longer a source of design constraints. The ADP3335 can be used with virtually any good quality capacitor and with no constraint on the minimum ESR. This innovative design allows the circuit to be stable with just a small $1 \mu \mathrm{~F}$ capacitor on the output. Additional advantages of the pole-splitting scheme include superior line noise rejecttion and very high regulator gain, which lead to excellent line and load regulation. Impressive $\pm 1.8 \%$ accuracy is guaranteed over line, load, and temperature.
Additional features of the circuit include current limit, thermal shutdown, and noise reduction.

## APPLICATIONS INFORMATION <br> OUTPUT CAPACITOR SELECTION

As with any micropower device, output transient response is a function of the output capacitance. The ADP3335 is stable over a wide range of capacitor values, types, and ESR (anyCAP). A capacitor as low as $1 \mu \mathrm{~F}$ is all that is needed for stability; larger capacitors can be used if high output current surges are anticipated. The ADP3335 is stable with extremely low ESR capacitors (ESR $\approx 0$ ), such as multilayer ceramic capacitors (MLCC) or organic semiconductor electrolytic capacitors (OSCON). Note that the effective capacitance of some capacitor types may fall below the minimum at extreme temperatures. Ensure that the capacitor provides more than $1 \mu \mathrm{~F}$ over the entire temperature range.

## INPUT BYPASS CAPACITOR

An input bypass capacitor is not strictly required, but is advisable in any application involving long input wires or high source impedance. Connecting a $1 \mu \mathrm{~F}$ capacitor from IN to ground reduces the circuit's sensitivity to PC board layout. If a larger value output capacitor is used, then a larger value input capacitor is also recommended.

## NOISE REDUCTION

A noise reduction capacitor $\left(\mathrm{C}_{\mathrm{NR}}\right)$ can be used, as shown in Figure 24, to further reduce the noise by 6 dB to 10 dB (Figure 22). Low leakage capacitors in the 100 pF to 1 nF range provide the best performance. Since the noise reduction pin, NR, is internally connected to a high impedance node, any connection to this node should be made carefully to avoid noise pickup from external sources. The pad connected to this pin should be as small as possible, and long PC board traces are not recommended.
When adding a noise reduction capacitor, maintain a minimum load current of 1 mA when not in shutdown.

It is important to note that as $\mathrm{C}_{\mathrm{NR}}$ increases, the turn-on time will be delayed. With NR values greater than 1 nF , this delay may be on the order of several milliseconds.


Figure 24. Typical Application Circuit

## THERMAL OVERLOAD PROTECTION

The ADP3335 is protected against damage from excessive power dissipation by its thermal overload protection circuit, which limits the die temperature to a maximum of $165^{\circ} \mathrm{C}$. Under extreme conditions (i.e., high ambient temperature and power dissipation) where die temperature starts to rise above $165^{\circ} \mathrm{C}$, the output current is reduced until the die temperature has dropped to a safe level. The output current is restored when the die temperature is reduced.

Current and thermal limit protections are intended to protect the device against accidental overload conditions. For normal operation, device power dissipation should be externally limited so that junction temperatures will not exceed $150^{\circ} \mathrm{C}$.

## CALCULATING JUNCTION TEMPERATURE

Device power dissipation is calculated as follows:

$$
P_{D}=\left(V_{I N}-V_{O U T}\right) I_{L O A D}+\left(V_{I N}\right) I_{G N D}
$$

Where $I_{L O A D}$ and $I_{G N D}$ are load current and ground current, and $V_{\text {IN }}$ and $V_{\text {out }}$ are input and output voltages, respectively. Assuming $I_{L O A D}=400 \mathrm{~mA}, I_{G N D}=4 \mathrm{~mA}, V_{I N}=5.0 \mathrm{~V}$, and $V_{\text {OUT }}=$ 3.3 V , device power dissipation is

$$
P_{D}=(5 \mathrm{~V}-3.3 \mathrm{~V}) 400 \mathrm{~mA}+5.0 \mathrm{~V}(4 \mathrm{~mA})=700 \mathrm{~mW}
$$

The junction temperature can be calculated from the power dissipation, ambient temperature, and package thermal resistance. The thermal resistance is a function not only of the package, but also of the circuit board layout. Standard test conditions are used to determine the values published in this data sheet, but actual performance will vary. For an LFCSP-8 package mounted on a standard 4-layer board, $\theta_{\mathrm{JA}}$ is $48^{\circ} \mathrm{C} / \mathrm{W}$. In the above example, where the power dissipation is 700 mW , the temperature rise above ambient will be approximately equal to

$$
\Delta T_{J A}=0.700 \mathrm{~W} \times 48^{\circ} \mathrm{C} / \mathrm{W}=33.6^{\circ} \mathrm{C}
$$

To limit the maximum junction temperature to $150^{\circ} \mathrm{C}$, the maximum allowable ambient temperature will be

$$
T_{A M A X}=150^{\circ} \mathrm{C}-33.6^{\circ} \mathrm{C}=116.4^{\circ} \mathrm{C}
$$

In this case, the resulting ambient temperature limitation is above the maximum allowable ambient temperature of $85^{\circ} \mathrm{C}$.

## PRINTED CIRCUIT BOARD LAYOUT CONSIDERATIONS

All surface-mount packages rely on the traces of the PC board to conduct heat away from the package. Use the following general guidelines when designing printed circuit boards to improve both electrical and thermal performance.

1. Keep the output capacitor as close as possible to the output and ground pins.
2. Keep the input capacitor as close as possible to the input and ground pins.
3. PC board traces with larger cross sectional areas will remove more heat from the ADP3335. For optimum heat transfer, specify thick copper and use wide traces.
4. It is not recommended to use solder mask or silkscreen on the PCB traces adjacent to the ADP3335's pins, since doing so will increase the junction-to-ambient thermal resistance of the package.
5. Use additional copper layers or planes to reduce the thermal resistance. When connecting to other layers, use multiple vias, if possible.

## LFCSP LAYOUT CONSIDERATIONS

The LFCSP package has an exposed die paddle on the bottom, which efficiently conducts heat to the PCB. In order to achieve the optimum performance from the LFCSP package, special consideration must be given to the layout of the PCB. Use the following layout guidelines for the LFCSP package.


Figure 25. $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ LFCSP Pad Pattern (Dimensions shown in millimeters)

1. The pad pattern is given in Figure 25. The pad dimension should be followed closely for reliable solder joints, while maintaining reasonable clearances to prevent solder bridging.
2. The thermal pad of the LFCSP package provides a low thermal impedance path (approximately $20^{\circ} \mathrm{C} / \mathrm{W}$ ) to the PCB. Therefore, the PCB must be properly designed to effectively conduct heat away from the package. This is achieved by adding thermal vias to the PCB, which provide a thermal path to the inner or bottom layers. See Figure 25 for the recommended via pattern. Note that the via diameter is small to prevent the solder from flowing through the via and leaving voids in the thermal pad solder joint.

Also, note that the thermal pad is attached to the die substrate, so the thermal planes to which the thermal vias connect must be electrically isolated or tied to $\mathrm{V}_{\mathrm{IN}}$. Do NOT connect the thermal pad to ground.
3. The solder mask opening should be about $120 \mu$ ( 4.7 mils ) larger than the pad size, resulting in a minimum $60 \mu \mathrm{~m}$ ( 2.4 mils) clearance between the pad and the solder mask.
4. The paste mask opening is typically designed to match the pad size used on the peripheral pads of the LFCSP package. This should provide a reliable solder joint as long as the stencil thickness is about 0.125 mm . The paste mask for the thermal pad needs to be designed for the maximum coverage to effectively remove the heat from the package. However, due to the presence of thermal vias and the size of the thermal pad, eliminating voids may not be possible.
5. The recommended paste mask stencil thickness is 0.125 mm . A laser cut stainless steel stencil with trapezoidal walls should be used. A "No Clean" Type 3 solder paste should be used for mounting the LFCSP package. Also, a nitrogen purge during the reflow process is recommended.
6. The package manufacturer recommends that the reflow temperature should not exceed $220^{\circ} \mathrm{C}$ and the time above liquidus is less than 75 seconds. The preheat ramp should be $3^{\circ} \mathrm{C} /$ second or lower. The actual temperature profile depends on the board density and must be determined by the assembly house as to what works best.

## SHUTDOWN MODE

Applying a TTL high signal to the shutdown ( $\overline{\mathrm{SD}}$ ) pin or tying it to the input pin, turns the output ON. Pulling $\overline{\mathrm{SD}}$ down to 0.4 V or below, or tying it to ground, turns the output OFF. In shutdown mode, quiescent current is reduced to a typical value of 10 nA .

## OUTLINE DIMENSIONS



ORDERING GUIDE

| Model $^{1}$ | Output Voltage (V) ${ }^{\mathbf{2}}$ | Temperature Range | Package Description | Package Option | Branding $^{3}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| ADP3335ACPZ-1.8-R7 | 1.8 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | $\mathrm{CP}-8-13$ | L1G |
| ADP3335ACPZ-2.5-R7 | 2.5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | CP-8-13 | L1H |
| ADP3335ACPZ-2.85R7 | 2.85 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | CP-8-13 | L1J |
| ADP3335ACPZ-3.3-R7 | 3.3 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | CP-8-13 | L1K |
| ADP3335ACPZ-3.3-RL | 3.3 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | CP-8-13 | L1K |
| ADP3335ACPZ-5-R7 | 5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead LFCSP_WD | CP-8-13 | L1L |
| ADP3335ARMZ-1.8-R7 | 1.8 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFA |
| ADP3335ARMZ-1.8-RL | 1.8 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFA |
| ADP3335ARMZ-2.5-RL | 2.5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFC |
| ADP3335ARMZ-2.5RL7 | 2.5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFC |
| ADP3335ARMZ-2.85R7 | 2.85 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFD |
| ADP3335ARMZ-2.85RL | 2.85 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFD |
| ADP3335ARMZ-3.3-RL | 3.3 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFE |
| ADP3335ARMZ-3.3RL7 | 3.3 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFE |
| ADP3335ARMZ-5-R7 | 5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFF |
| ADP3335ARMZ-5-REEL | 5 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | LFF |

${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.
${ }^{2}$ For additional voltage options, contact a local sales or distribution representative.
${ }^{3} \mathrm{Z}=$ RoHS Compliant Parts have a "\#" marked on the device preceding the date code.

NOTES
Data Sheet ADP3335

NOTES

## NOTES


[^0]:    ${ }^{1} \mathrm{~V}_{\text {IN }}=2.6 \mathrm{~V}$ to 12 V for models with $\mathrm{V}_{\mathrm{OUT}(\mathrm{NOM})} \leq 2.2 \mathrm{~V}$.

